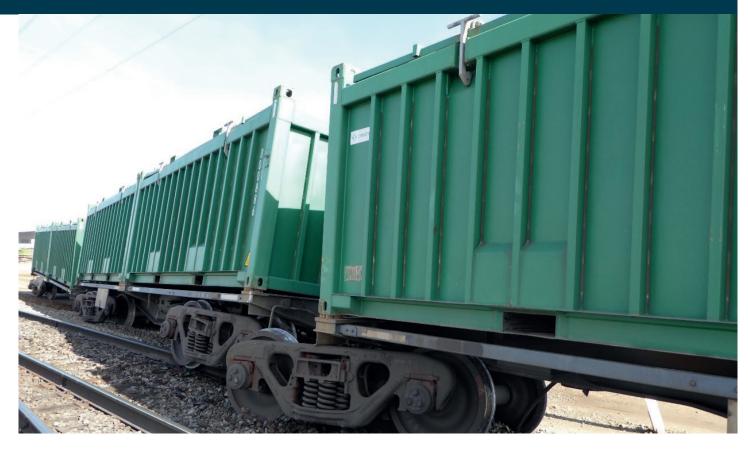


Australian Government Australian Transport Safety Bureau

Derailment of freight train 1501S

Near Dry Creek, South Australia | 28 July 2017



Investigation

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Addendum

Page	Change	Date

Safety summary

What happened

At about 0617 on 28 July 2017, a Bowmans Intermodal containerised ore train (1501S) travelling empty from Port Flat, South Australia (SA) stopped at Dry Creek South in SA. The driver felt the performance of the train 'very sluggish', as it was not rolling as it had prior to rounding a curve on the approach to Dry Creek South. The train crew notified the Australian Rail Track Corporation (ATRC) network control officer at Mile End, SA of their situation and that they intended to inspect their train. A short time later, the train crew confirmed to the network control officer that the last three wagons from 1501S had derailed. The train crew were uninjured. However, there was substantial damage to the wagons, track and signalling infrastructure.

What the ATSB found

The ATSB found a vertical split head defect had developed undetected from imperfections introduced during the manufacture of the rail 90 years ago. The defect propagated vertically and longitudinally, roughly through the centre line of the lower leg rail in the curve approaching Dry Creek South.

The passage of a previous train (1122) over this section of track caused an initial rail break, affecting the integrity of the rail and electrical continuity of the associated track circuit, which prevented a signal from clearing for the next train (1501S). The network control officer authorised the driver to pass the signal at stop, with the condition that the train travel at low speed.

However, the rail break was not visually obvious to the train crew as the locomotive rounded the curve. As the rear of that train passed over the break, a 2 m section of rail fragmented causing the last three wagons to derail.

Detailed (ultrasonic) inspection of the track about one month prior to the occurrence recorded a sustained loss of back wall echo at the derailment location, automatically marking the rail with a spray of paint. However, the ultrasonic inspection operator attributed the recorded event to the poor surface condition of the railhead, which is a common condition that can inhibit the testing. There was no retesting initiated or surface condition report lodged in response to the recorded event. The absence of any follow-up missed an opportunity to identify the presence of the vertical split head defect prior to the rail fracture and the subsequent derailment of 1501S.

What's been done as a result

Following the incident, Speno implemented a review of testing techniques used by operators where poor surface condition exists and the procedures for reporting and testing of rail affected by surface condition.

The Australian Rail Track Corporation reaffirmed the adequacy of the Track and Civil Code of Practice for ultrasonic inspections and the reporting requirements in accordance with contractual arrangements with the ultrasonic inspection operator. The rail in the Dry Creek area is programmed for replacement during 2018 as part of the Adelaide to Tarcoola Re-Railing Project.

Safety message

Defects can develop in rails (and welds) due to a wide range of reasons. Early detection and treatment of a defect that could cause a fracture of the rail is of major importance. While poor surface condition of the railhead is a known limit to the effectiveness of ultrasonic testing, its presence can mask internal track defects, particularly when the condition exists over an extended area. If an inspection cannot test or can only partly test rails, maintenance personnel must report

the shortfall to highlight operational risk and the requirement for a timely supplementary examination.



Fractured rail section in lower rail of curve

Source: ATSB

The occurrence

At about 0145 on the 28 July 2017, a Bowmans Rail freight train (1501S) was prepared for departure from Port Flat near Adelaide, South Australia (Figure 1). Train 1501S was an empty containerised ore service comprised of two locomotives (GL108 leading, CM3308 trailing) and 56 wagons. The train was 802 m long, with a trailing mass of 1,283 t and crewed by two drivers. The train was to travel via Dry Creek in South Australia to the Bemax Siding located between Thackaringa and Kanandah in New South Wales.

At about 0548, the driver of 1501S contacted the Australian Rail Track Corporation (ARTC) network control officer (NCO) located at Mile End in South Australia to advise that they were ready to depart Port Flat. The NCO notified the driver that they would travel under signal indication up to Signal 1 at Dry Creek, where a Train Authority¹ would be required for train 1501S to proceed. The NCO was unable to clear signal 1 to a proceed indication,² as a track circuit³ had remained occupied following the passage of the previous train (1122) about 30 minutes earlier.



Figure 1: Location of the derailment of Train 1501S in South Australia

Source: Geoscience Australia annotated by ATSB

Any signal indication other than stop.

An instruction in the prescribed format issued by the train controller in connection with the movement of a train.

An electric circuit that uses the rails of a railway as conductors such that a train electrically connects them via its axles. The absence or presence of this rail-to-rail connection indicates the absence or presence of a train or item of rollingstock.

At about 0608, the train crew stopped train 1501S at signal 1, and the NCO issued the train authority for the crew to pass the signal at stop. The NCO included instructions for the train crew to proceed at low speed and stop at the points⁴ to ensure they were set correctly for the route to the next fixed signal⁵ (signal 5). After confirming the content of the train authority with the NCO, the driver passed signal 1 and continued toward Dry Creek South, controlling train 1501S to maintain a speed below 25 km/h.

The driver recalled that when travelling about half way around the curve between signals 1 and 5 he felt the lead locomotive pass over a dip in the left (lower leg) rail. A short time later, train performance 'felt very sluggish' and it was not running as it was prior to the curve. At the time, the lead locomotive (GL108) was travelling at about 17 km/h. At about 0617, the driver contacted the NCO, and advised that train 1501S had stopped at Dry Creek South and that they would inspect the train.

At about 0626, an ARTC signal maintainer arrived onsite to investigate the cause of an earlier reported fault; that is, signal 1 not clearing. Shortly after, the signal maintainer contacted the NCO advising that the rear of train 1501S had derailed and there was substantial damage to the wagons, track, location case⁶ and other signalling infrastructure (Figure 2).



Figure 2: Derailed rear three wagons of 1501S and damaged signal 5 location case

Source: ATSB

At about 0627, the driver of train 1501S contacted the NCO confirming that the last three wagons (CQYY 3264-G, CQYY 3261-C and CQYY 3265-P) had derailed. The wagons had travelled about 285 m in a derailed state before train 1501S stopped.

⁴ A set of points permits rail traffic to change from one track to another. Points are normally referred to as left or right hand denoting the turnout direction as viewed from the toe end.

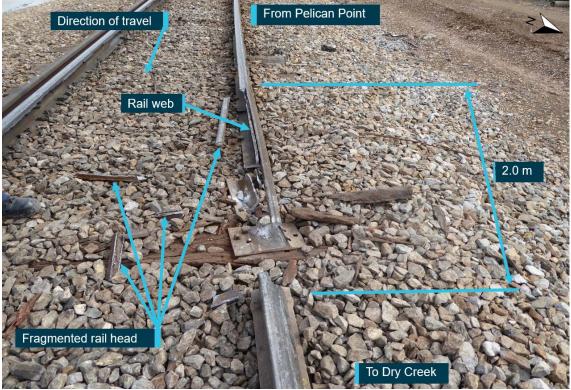
⁵ A manually or power operated signal which is permanently located near the line.

⁶ Signalling lineside apparatus housings at a particular site and the equipment contained therein.

Site inspection

An inspection of the track identified a 2 m section of rail had fractured, on the lower leg of the left curve (Figure 3).

Figure 3: Fractured section of rail



Source: ATSB

The railhead had split vertically and longitudinally, roughly through the centre line of the rail in the affected section. The split propagated through to the head/web transition region and outward through the railhead toward the gauge side of the rail, separating the head from the web⁷ (Figure 4).

The web had also fractured at several points through the affected section. These breaks were predominately vertical through the web, and transverse in the foot of the rail. The breaks through the web were due to overstress, which probably occurred during the passage of the previous train 1122, and the subsequent passage of 1501S that derailed.

⁷ That part of the rail between the head and the flange (foot).



Figure 4: Vertical split head section

Source: ATSB

Passing signal 1 at stop

The ARTC *Code of Practice, Volume 3* (CoP) defines the operations and safe working rules for managing train movement⁸ through the Dry Creek area. Before authorising the crew of a train to pass a signal at stop, the CoP required the NCO, and train crew, to assess the situation including:

- why the signal is at stop
- if the section is clear or occupied
- if the track is safe or unsafe
- the conditions to be included in the Train Authority to authorise the train to pass the signal at stop.

Track circuits in the Dry Creek area used the rails and other signalling equipment as conductors to form an electric circuit. The presence of a train or other rollingstock, or a break in the electrical continuity of the circuit, will cause the track circuit to signal an occupancy.

In this case, the signal was at stop due to an indication the track section remained occupied following the movement of the previous train (1122). A track section might indicate as occupied due to a number of reasons, such as an obstruction, faulty equipment, broken electrical connections, or as in this case, a broken rail.

When travelling on a track section indicated as occupied, there is an increased risk that the train may encounter an obstruction, points incorrectly set for the intended route, or other equipment not operating as expected (for example, level crossings). Consequently, when authorising a train to

⁸ The operation on rail of a train or other track vehicle or machine.

pass the signal at stop, an NCO should apply conditions to ensure appropriate management of these risks.

Prior to authorising the train crew to pass signal 1, the NCO communicated to the train crew that a track circuit in the route was indicating an occupancy, preventing the signal from clearing. There was no further discussion related to the safety of the track. However, the NCO issued conditions in the train authority for the driver to proceed past signal 1 at low speed and for the train to stop at points to ensure they were set correctly for the intended route. The CoP defined low speed as a speed which will enable a train movement to be stopped within half the distance that the track is seen to be clear ahead, but does not exceed 25 km/h.

Typically, a simple rail break would not result in a derailment, especially if a train is travelling at low speed. This is because, as in this case, the CoP also required a train crew to maintain vigilance by being alert, observing the track (including rails) in the direction of the movement, and being prepared to stop or reduce train speed if required.

Train 1501S passed signal 1 about an hour before sunrise. The driver continued at speeds below 25 km/h, travelling approximately 1,290 m toward Dry Creek South before stopping. Although the driver reported to the NCO that the locomotive dipped to the left when rounding the curve, the train crew did not report observing any significant anomaly with the track and were likely unaware that a rail had broken.

The locomotives and all wagons with the exception of the last three remained on the track. It is likely the rail disintegrated during the passage of one of the last two wagons (CQYY 3261-C or CQYY 3265-P) over the failed section of track. The derailment of the last two wagons likely pulled the rear bogie of the third to last wagon, CQYY 3264-G from the track. The rear of train 1501S travelled about 285 m from the point of derailment (break in the rail) before stopping.

Track inspection arrangements

The ARTC *Track and Civil Code of Practice – Rail*, defines the guidelines for the scheduled inspection the assessment of rail and rail wear. The scheduled inspections included:

- A patrol inspection of the rail for visible defects and conditions (i.e. indications of a defect) that may affect the integrity of the track structure, including the following:
 - broken rails and rail welds
 - rail and rail weld deformations and discontinuities
 - wheel burns
 - damage to rail surface or section
 - unusual patterns of gauge face contact
 - unusual vehicle tracking patterns
 - rail corrugation
 - rail crippling
 - other obvious indications of defects (e.g. bleeding).⁹

The patrol inspections were typically carried out from an on-rail vehicle travelling at a speed consistent with the inspection or by walking. Where track circuits were installed, these could also be employed as an additional method to detect rail failures (such as a break). Patrols conducted two type of inspections:

- A general inspection to visually inspect new welds or where the response following detection of a rail or weld defect is to 'observe'.
- A detailed inspection, carried out through continuous or manual ultrasonic rail flaw detection.

⁹ Discolouration on the web due to the movement of oxides to the surface.

Continuous and manual ultrasonic rail flaw detection involved passing sound waves into the rail and monitoring the echo returned by the sound waves reflecting off internal and external surfaces (reflectors). Defects within the rail create reflectors that return echo patterns depending on their type, location and size. Examination of the reflectors enables a skilled operator to deduce the existence, type and size of a suspected rail defect.

The ARTC *Civil Technical Maintenance Plan ETE-00-03* sets out the routine inspection tasks and minimum inspection frequency for the track and civil infrastructure (Table 1).

Type of inspection	Infrastructure element	Description	Minimum Frequency	Conducted by
Track patrol inspection (By road /rail vehicle or by walking)	Rails and Joints	Includes: Rail; New Welds; Mechanical and insulated Joints; Rail wear; Lubrication	1 Patrol / 7 days (1 day latitude)	Track inspector
Rail detailed inspection	Rail - internal	Continuous ultrasonic rail flaw inspection or manual hand-held inspection where continuous inspection is not effective	At least every 15 MGT ¹⁰	-

Table 1: Summary from Technical Maintenance Plan – Track System

Source: ARTC modified by ATSB

Track Patrol inspection

The ARTC standard for *Track Patrol, Front of Train, General and Detailed Inspections* specifies the scope and methodology for the performance of this inspection. The standard recognises the track patrol is principally:

A visual inspection intended to detect obvious, abnormal conditions. It is unlikely that hidden failures or conditions that don't have a significant visual impact will be detected by Track Patrol which is typically performed from a hi-rail vehicle at moderate speed. Other scheduled (and ad-hoc) general and detailed inspections focus on specific components or conditions and are intended to detect these less obvious defects.

On 27 July 2017, the day preceding the derailment of 1501S, the ARTC track inspector completed a track patrol inspection for the section of rail between the Dry Creek Triangle¹¹ and Pelican Point. The track inspector did not record observing any anomaly in the rail condition through the area where the derailment occurred.

Continuous ultrasonic rail flaw inspections

ATRC's technical maintenance plan specified the minimum frequency for a detailed inspection (ultrasonic rail flaw inspection) was at least every 15 MGT. Although the track section between the Dry Creek Triangle and Pelican Point carried around 7 - 10 MGT per annum, ARTC scheduled the detailed inspections yearly.

ARTC undertook the detailed inspections in the Dry Creek Triangle to Pelican Point section through a contractual arrangement with Speno Rail Maintenance Australia (Speno). The Speno

¹⁰ Million Gross Tonnes.

¹¹ Dry Creek Triangle includes the track section between signal 1 and signal 5.

Site Safety, Environmental & Quality Management Plan ARTC - Rail Flaw Detection, detailed the specific requirements for Speno accessing the rail network and the rail testing process undertaken.

The rail testing process typically involved the operation of two on-track vehicles. For this type of operation, a main test vehicle (Figure 5) would conduct continuous testing where the ultrasonic operator would interpret, mark and log ultrasonic events displayed on the test vehicles display monitors. Automatic paint guns sprayed a white paint mark on the gauge side, rail web and foot of each rail when the system detected the presence of a defined event.

Following the identification of an event, the operator in the main test vehicle relayed information to a following vehicle, where an operator in that vehicle was responsible for manual ultrasonic testing to localise, identify, size and assess the detected flaw in accordance with the relevant ARTC standards.

The ARTC *Manual for Non-Destructive Testing of Rail, ETN-01-04* included specifications for the ultrasonic test equipment and the types and sizes of rail flaws for detection. The manual required the ultrasonic operators to use a range of probes when inspecting the rail and welds for cracks and similar discontinuities. The main test vehicle used in testing the rail in the Dry Creek area towed the roller search unit equipped with an array of 0°, 38° and 70° probes (Figure 5). The arrangement of the probes enabled continuous inspection of each rail leg for defects in various orientations.

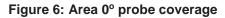


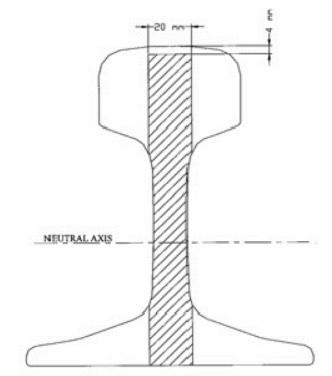
Figure 5: FL-18 (RFAS-2100) rail analysis system (main test vehicle)

Source: Speno Rail Maintenance Australia, annotated by ATSB

The 0° probe examined the full rail depth, including welds (Figure 6). Defects located by this probe include bolt hole cracks and longitudinal defects of a horizontal nature in the railhead, web and foot. However, vertical defects are more difficult to detect by continuous ultrasonic testing of rail, since the vertical surface of the defect is less likely to provide a clear reflection from any probe.

While the presence of a vertical split head defect may not display as a distinctive signature in the reflected signal on the operators screen, there are signature patterns that may indicate a potential issue. A vertical defect in the railhead may present as a loss of back wall echo (LBWE), where the signal from the 0° probe is deflected, thereby causing the reflected signal from the base of the rail (foot) to drop below a pre-defined level.





Source: Australian Rail Track Corporation

A loss of signal from the bottom of the rail, over any length greater than 4 mm is displayed to the operator in the raw data. A loss of signal over 50 mm will activate an audible signal to the operator that has a unique tone dependent on the respective rail and display the LBWE as a length value to the operator. The pulse echo reliant transducers also activate the automatic paint guns spraying location marks on the rail web. Any ultrasonic shielding (LBWE) or anomalous indication should trigger a localised visual inspection and manual ultrasonic scanning from other faces of the rail to investigate.

The ARTC standard, *Non-Destructive Testing of Rail ETE-01-03* detailed the response actions and timeframe to levels of shielding and testability of rail (Table 2).

Shielding level	Purpose of assessment	Definition	Response time(s)	Action(s)
Minor	Require test car to re-test at low speed	 Any of the following testing at normal speed Vehicle had to reduce speed LBWE greater than 50 mm More than one LBWE per m Line difficult to test 	Immediately 7 days	Stop, examine rail to identify cause of loss of detection Re-test at 5 km/h Test car shall report shielding
Moderate	Report early stages for remediation or	Any of the following testing at reduced speed • LBWE between 50 and 200 mm	3 days	Test car shall report shielding Rectification within timeframes specified in

Table 2: Summary from standard, non-destructive testing of rail

	remediation planning	If rail difficult to test		Corridor Management Plan
Major	Require hand testing if test car cannot test	 Any of the following testing at reduced speed LBWE greater than 200 mm More than one LBWE per m One or more probes giving inconsistent results 	7 days 1 day	Test affected rail by hand or apply Track Speed Restriction as required Test car shall report shielding

Source: ARTC modified by ATSB

The continuous ultrasonic inspection was undertaken on 26 June 2017, about one month prior to the derailment of train 1501S. There was no ultrasonic reflector indicating a vertical split head defect. However, there were occasions of intermittent LBWE and a prolonged period of LBWE over about 2 m that coincided with the derailment location (Figure 7). The inspection also indicated the presence of spurious reflectors from the 70° shear wave transducers. These reflectors likely emanated from the poor rail surface condition that often occurs when the roller search unit is having difficulty maintaining continuity with the rail.



Figure 7: Ultrasonic signatures at derailment location on 26 June 2017

Source: Speno Maintenance Australia, annotated by ATSB

Following the derailment, Speno reviewed replays and examined the ultrasonic signatures from other track structures (insulated joints and boltholes) taken in the area and confirmed the ultrasonic testing system in the main test vehicle was operating within normal parameters at that time.

Examination of the replays also suggested that the operator was having trouble (on occasion) in maintaining continuity of the roller search unit with the rail surface during the run. To compensate, the operator of the test vehicle was undertaking the testing at a reduced speed of 5 km/h, as specified in the response actions of the ARTC procedure.

The Speno rail analysis unit was equipped with audible alarms and paint spray guns that flagged the LBWE event as an exceedance and marked the rail during the ultrasonic inspection of the 26 June 2017 (Figure 8).

The prolonged LBWE event and continued difficulty experienced in testing should have triggered the next level of response action. If rail could not be tested or only partly tested, due to ultrasonic shielding, ARTC required the operator to test the affected area by hand or to forward a *Rail Surface Condition Report* detailing the circumstances that impeded the testing. Neither a response action nor a condition report was initiated in this case.



Figure 8: Failed section of railhead showing markings from ultrasonic car testing

Source: ATSB and ARTC (inset photograph)

The previous ultrasonic test of rail in the Dry Creek area occurred in May of 2016. This test also recorded an intermittent LBWE in the same vicinity. Prolonged periods of LBWE also occurred on the opposite rail (Figure 9) illustrated at the 0.226 km mark. Similarly, there was also no record of retesting or the lodgement of a surface condition report. It is likely that the operator on this occasion also assessed the spurious reflectors and LBWE were, in the absence of defined defect signatures, due to the poor surface condition of the railhead.



Figure 9: Ultrasonic signatures at 0.226 km point 04 May 2016

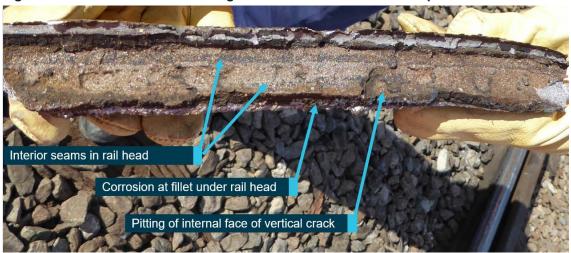
Source: Speno Maintenance Australia, annotated by ATSB

Safety analysis

The rail installed in the lower leg of the curve at the Dry Creek North Fork displayed the manufacturer brand, AS BHP Co Ltd 1X27 100LBS OH. The branding indicates the manufacture date was in 1927, from an open-hearth (OH) furnace process. Older rails, produced by means of OH furnaces and cast into ingots, generally exhibited higher levels of impurities than rails produced through the current continuous casting process.¹²

The rail at the derailment site was installed in 1999. The running surface of the rail at the derailment location and in the curve exhibited rolling contact fatigue (RCF) defects that developed from shear stresses at the rail-wheel interface. The presence of RCF defects such as plastic flow, flaking and minor spalling, can mask the signal during ultrasonic inspection and hence prevent the detection of larger and deeper defects that may be present within the railhead.¹³

On-site examination of the section of rail showed evidence of an internal seam extending vertically within the centreline of the railhead. The seam surfaces were heavily corroded and punctuated by an elongated band of inclusions and oxidation located at a depth of around 10 mm from the running surface of the railhead (Figure 10). The general appearance and orientation of the inclusion banding indicated that it was pre-existing and very likely to have been produced when the rail was cast at the time of manufacture. Fatigue cracking had developed from the inclusion bands and had then propagated toward the railhead-running surface and the web transition region, creating a 'vertical split head'. Typically, longitudinal crack propagation is influenced by a combination of increasing axle loads, wheel impacts or eccentric loading on a railhead exhibiting a flattened profile.





Source: ATSB

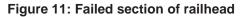
The vertical split head in this instance propagated undetected into a critical defect of around 2 m in length. The defect exhibited the typical visual indicators of well-developed dark oxide streaking on the centreline of the running surface and oxide streaks (bleeding) on the fillet area of the rail web under the defect (Figure 11). The forces exerted by the passage of train 1501S across the area of rail containing the vertical split defect (and broken rail) resulted in the fragmentation of that section of rail. The disruption of the rail running surface then led to the derailment of the last three wagons of train 1501S.

¹² Vertical split head defects – some insights into their development and growth, Stephen Marich and Malcom Kerr, RTSA Conference on Railway Engineering, Darwin 20-30 June 2004, p 21.3

¹³ Rail defect handbook RC2400, Australian Rail Track Corporation Issue A, Revision 0, March 2006, p29

Track inspection

As neither the scheduled track patrol nor ultrasonic inspection identified the presence of a defect, it cannot be determined when the vertical split defect first propagated towards a critical size. The yearly ultrasonic inspection is heavily reliant on the ability of the individual operator to detect and interpret anomalies in the rail infrastructure (or displayed ultrasonic signatures) that signal the presence of a potential defect.





Source: ATSB

The continuous inspection of rail infrastructure by track patrol or ultrasonic test vehicles typically involves the operator undertaking repetitive tasks in scanning the track structures (or visual display screens) for anomalies while operating a vehicle or other on-board equipment over long sections of track. Track patrols undertaken from road-rail vehicles target the identification of abnormal conditions that may affect the integrity of the infrastructure or operation of rollingstock. Defects that do not have a significant visual impact may be overlooked, increasing the reliance on the detailed inspections to detect hidden conditions.

The Australian Rail Track Corporation (ARTC) also recognised that the non-destructive testing used in undertaking the detailed inspections did not assure detection of all defects due to limitations of existing ultrasonic techniques.

To minimise the risk of a missed defect, ARTC required the ultrasonic testing process, and in particular the conditions in the testing vehicle, be optimised to facilitate the concentration of the operator on the data being analysed. This included:

- · the judicious use of post analysis facilities of recorded data
- in-car working conditions and temperature
- computer screens that are adequately protected from sun glare
- monitoring that the speed of the car is compatible with the ability to analyse data presented

- safe working practices are adequately catered for outside the time allowed for test analysis
- fatigue management of operators (consideration of rotation of operators with hand testers)
- undue pressure on time allowed in section
- peer development and regular training in compliance with this document
- monitoring of operators' performance in terms of percentage of defect identified.

On the 26 June 2017, Speno Rail Maintenance Australia (Speno) commenced the ultrasonic inspection of track at Pelican Point and then proceeded towards Dry Creek. Speno identified that the inspection run at Dry Creek through the area of the derailment would therefore have occurred at about 1645, toward the end of the operators shift. However, there was no further evidence to suggest that fatigue contributed to a failure to detect a rail defect.

The rail in the area of the derailment and a number of other areas along this section of track was in relatively poor condition and exhibited heavily flowed head¹⁴ with severe flaking¹⁵ on the rail surface. The condition of the railhead probably resulted in the failure of the roller search unit to maintain effective contact with the rail surface during the run, either producing spurious reflectors or inhibiting transmission of ultrasonic signals from a defect.

The operator did not follow-up the loss of back wall echo (LBWE) trace and alarm in the area of the derailment by triggering a localised ground inspection or forwarding a rail surface condition report to ARTC.

The generally poor condition of the track in the area of the derailment meant the operator received many spurious ultrasonic reflectors and alarms while traversing that track section. It is likely that the operator's assessment of the importance of the indications decreased relative to the rail condition, track category and test frequency. Consequently, the operator attributed the LBWE indications to surface condition, rather than the presence of a defect.¹⁶

¹⁴ Rolling out of the metal of the head towards the sides without a breaking down of the underside of the head.

¹⁵ A condition that occurs on the running surface appearing as a mosaic like pattern of small cracks.

¹⁶ Speno Broken rail report CTT 2014-016, 8 August 2017.

Findings

From the evidence available, the following findings are made with respect to the derailment of freight train 1501S near Dry Creek on the 28 July 2017. These findings should not be read as apportioning blame or liability to any particular organisation or individual.

Contributing factors

- An undetected defect resulted in the formation of a longitudinal fracture within the railhead that propagated both longitudinally and vertically (parallel to the side of the head).
- The forces exerted by the passage of train 1501S across the area of rail containing the vertical split defect (and broken rail) resulted in the fragmentation of a 2 m section of rail. The disruption of the rail running surface resulted in the derailment of the last three wagons of train 1501S.

Other factors that increased risk

 The operator undertaking ultrasonic testing of rail at Dry Creek North Fork on 26 June 2017 assumed the reflectors recorded resulted from the poor surface condition of the railhead and did not follow-up the loss of back wall echo indication that occurred at the location of the rail break.

Other findings

• The passage of a previous train (1122) across the section of rail containing the vertical split defect likely caused the rail to break, further reduced the integrity of the track to support the passage of rollingstock at this location.

Safety actions

Whether or not the ATSB identifies safety issues in the course of an investigation, relevant organisations may proactively initiate safety action in order to reduce their safety risk. The ATSB has been advised of the following proactive safety action in response to this occurrence

Proactive safety action taken by Speno Rail Maintenance Australia

Following the incident, Speno Rail Maintenance Australia investigated the broken rail occurrence and implemented a review of testing techniques used by operators in areas where poor surface condition exists and the implementation of procedures for reporting and testing of rail affected by surface condition.

Proactive safety action taken by Australian Rail Track Corporation

Following the incident, the Australian Rail Track Corporation (ARTC) addressed with Speno the reporting arrangements required in accordance with the contract between the two parties. Additionally ARTC reaffirmed the adequacy of the Track and Civil Code of Practice in relation to ultrasonic inspections.

The rail in the Dry Creek area is programmed for replacement during 2018 as part to the Adelaide to Tarcoola Re-Railing Project.

General details

Occurrence details

Date and time:	28 July 2017 – 0617 ACST		
Occurrence category:	Incident		
Primary occurrence type:	Derailment		
Location:	Dry Creek South		
	Latitude: 34° 50.287' S	Longitude: 138° 34.95' E	

Train details

Train operator:	Bowmans Rail	
Registration:	1501S	
Type of operation:	Freight	
Persons on board:	Crew – 2	Passengers – 0
Injuries:	Crew – 0	Passengers – 0
Damage:	Substantial	

Sources and submissions

Sources of information

The sources of information during the investigation included the:

- Australian Rail Track Corporation
- Bowmans Rail
- Speno Rail Maintenance Australia

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Vertical split head defects – some insights into their development and growth, Stephen Marich and Malcom Kerr, RTSA Conference on Railway Engineering, Darwin 20-30 June 2004, p 21.3

Submissions

Under Part 4, Division 2 (Investigation Reports), Section 26 of the *Transport Safety Investigation Act 2003* (the Act), the Australian Transport Safety Bureau (ATSB) may provide a draft report, on a confidential basis, to any person whom the ATSB considers appropriate. Section 26 (1) (a) of the Act allows a person receiving a draft report to make submissions to the ATSB about the draft report.

A draft of this report was provided to the Australian Rail Track Corporation, Bowmans Intermodal, Speno Rail Maintenance Australia and the Office of the National Rail Safety Regulator.

Submissions were received from the Australian Rail Track Corporation, Speno Rail Maintenance Australia and the Office of the National Rail Safety Regulator. The submissions were reviewed and where considered appropriate, the text of the report was amended accordingly.

Australian Transport Safety Bureau

The Australian Transport Safety Bureau (ATSB) is an independent Commonwealth Government statutory agency. The ATSB is governed by a Commission and is entirely separate from transport regulators, policy makers and service providers. The ATSB's function is to improve safety and public confidence in the aviation, marine and rail modes of transport through excellence in: independent investigation of transport accidents and other safety occurrences; safety data recording, analysis and research; fostering safety awareness, knowledge and action.

The ATSB is responsible for investigating accidents and other transport safety matters involving civil aviation, marine and rail operations in Australia that fall within Commonwealth jurisdiction, as well as participating in overseas investigations involving Australian registered aircraft and ships. A primary concern is the safety of commercial transport, with particular regard to operations involving the travelling public.

The ATSB performs its functions in accordance with the provisions of the *Transport Safety Investigation Act 2003* and Regulations and, where applicable, relevant international agreements.

Purpose of safety investigations

The object of a safety investigation is to identify and reduce safety-related risk. ATSB investigations determine and communicate the factors related to the transport safety matter being investigated.

It is not a function of the ATSB to apportion blame or determine liability. At the same time, an investigation report must include factual material of sufficient weight to support the analysis and findings. At all times the ATSB endeavours to balance the use of material that could imply adverse comment with the need to properly explain what happened, and why, in a fair and unbiased manner.

Developing safety action

Central to the ATSB's investigation of transport safety matters is the early identification of safety issues in the transport environment. The ATSB prefers to encourage the relevant organisation(s) to initiate proactive safety action that addresses safety issues. Nevertheless, the ATSB may use its power to make a formal safety recommendation either during or at the end of an investigation, depending on the level of risk associated with a safety issue and the extent of corrective action undertaken by the relevant organisation.

When safety recommendations are issued, they focus on clearly describing the safety issue of concern, rather than providing instructions or opinions on a preferred method of corrective action. As with equivalent overseas organisations, the ATSB has no power to enforce the implementation of its recommendations. It is a matter for the body to which an ATSB recommendation is directed to assess the costs and benefits of any particular means of addressing a safety issue.

When the ATSB issues a safety recommendation to a person, organisation or agency, they must provide a written response within 90 days. That response must indicate whether they accept the recommendation, any reasons for not accepting part or all of the recommendation, and details of any proposed safety action to give effect to the recommendation.

The ATSB can also issue safety advisory notices suggesting that an organisation or an industry sector consider a safety issue and take action where it believes it appropriate. There is no requirement for a formal response to an advisory notice, although the ATSB will publish any response it receives.

Australian Transport Safety Bureau

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vestigation

ATSB Transport Safety Report

Rail Occurrence Investigation Derailment of freight train 1501S

Near Dry Creek, South Australia on 28 July 2017

RO-2017-008 Final – 31 October 2018